

# Series Expansions from Corner Transfer Matrices: The Square Lattice Ising Model

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*Received February 6, 1979*

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The corner transfer matrix formalism is used to obtain low-temperature series expansions for the square lattice Ising model in a field. This algebraic technique appears to be far more efficient than conventional methods based on combinatorial enumeration.

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**KEY WORDS:** Lattice models; series expansions; corner transfer matrices.

## 1. INTRODUCTION

Exact series expansions have been of considerable importance in the investigation of the critical behavior of lattice models in statistical mechanics. In spite of the large number of techniques which have been devised, the derivation of significant numbers of series coefficients is a formidable problem. Most techniques are based on combinatorial enumeration ("graph-counting") and the number of series terms which can be obtained is limited mainly by the rate at which graph embeddings can be counted using digital computers. The present paper describes an algebraic technique for obtaining series expansions for various Ising models on the square lattice using an algebraic method based on the work of Baxter<sup>(1)</sup> (hereafter referred to as I). Wortis<sup>(2)</sup> has commented that the most efficient techniques for obtaining series expansions tend to replace combinatorial complexity by algebraic complexity.

Baxter<sup>(1,3)</sup> has described a hierarchy of variational approximations for the partition functions of lattice models. The approximations involve matrix expressions for the eigenvectors of the transfer matrix. The lowest order approximation (using  $1 \times 1$  matrices) is that described by Kramers and Wannier,<sup>(4)</sup> who showed that the approximation gives the first few series

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coefficients correctly. As  $n \rightarrow \infty$  the formalism becomes exact and the equations [(1a)–(1c)] are the variational expressions for the corner transfer matrices described by Baxter.<sup>(5,6)</sup>

Throughout this paper we work with the exact equations, which involve infinite matrices. Fortunately, for the purposes of obtaining a finite number of coefficients in the series expansion of the reduced partition function  $\kappa$ , only a small number of rows and columns of the matrices need be considered explicitly. This reduction does depend on choosing an appropriate basis for the matrices.

The following sections outline the procedures for obtaining series expansions for  $\kappa$  from the corner transfer matrix equations. The low-temperature expansion for the square lattice Ising model in a magnetic field is considered as a test case.

Section 2 describes the variational expressions for the (infinite) corner transfer matrices (as given in I) and shows how the matrix equations can be transformed into a more unified form. In obtaining solutions of the equations we are at liberty to change the basis, specify various normalization conditions, and introduce various scale factors. We make use of all these “degrees of freedom” to simplify the calculations. Section 3 carries out the iterative solution of the equations for the nearest-neighbor Ising model, using the procedure described in I, but expressing the results as a power series. This example exhibits an important general property, namely that the equations are dominated by certain leading order terms and so it is possible to obtain the leading power of the eigenvalues of the corner transfer matrices explicitly as described in Section 4. This result forms the basis for a considerable simplification of the iterative procedure. This is described in Section 5, which gives a complete specification of which matrix equations can be used to solve for any required matrix element. Once this is known it is possible to work through the equations iteratively, obtaining solutions for the leading powers of the matrix elements. Once the leading powers are known, the equations can be examined to determine the order to which a matrix element must be obtained if some other matrix element is to be given to a specified order. These procedures are outlined in Section 6. They form the basis for the sequence of computations described in Sections 8 and 9. (Section 7 describes, for completeness, the precise way in which we have transformed the equations to simplify the calculations. These transformations are purely for computational convenience and do not affect the structure described in Sections 5 and 6.)

The results tabulated in the appendix show that the algebraic technique is particularly efficient. We have been able to expand the reduced partition function  $\kappa$  to order 23 in the low-temperature variable  $u$ . The longest series previously obtained extended only to  $u^{11}$  (Sykes *et al.*<sup>(7)</sup>). Similar series

expansion techniques should be possible for other square lattice models. These are currently under investigation.

## 2. THE MATRIX EQUATIONS

The variational equations for the corner and half-row transfer matrices are given in Eq. (30) of I. For an isotropic system they are

$$\sum_b F(a, b)A^2(b)F(b, a) = \xi A^2(a) \quad (1a)$$

$$\begin{aligned} \sum_{b,b'} w(a, b, a', b')F(a, b)A(b)F(b, b')A(b')F(b', a') \\ = \eta A(a)F(a, a')A(a') \end{aligned} \quad (1b)$$

$$A^T(a) = A(a), \quad F^T(a, b) = F(b, a) \quad (1c)$$

Here  $a, b, a'$ , and  $b'$  have values  $+1$  and  $-1$ ; each of  $F(+, +)$ ,  $F(+, -)$ ,  $F(-, +)$ ,  $F(-, -)$ ,  $A(+)$ ,  $A(-)$  is a matrix;  $\xi$  and  $\eta$  are positive real numbers; and  $w(a, b, a', b')$  is the Boltzmann weight of a face of the square lattice with spins  $a, b, a'$ , and  $b'$  at the bottom left, bottom right, top left, and top right corners, respectively. Thus the partition function  $Z$  is

$$Z = \sum_{\sigma} \prod_i w(\sigma_i, \sigma_j, \sigma_k, \sigma_l) \quad (2)$$

where the product is over all faces  $(i, j, k, l)$  of the lattice and the sum is over the value  $+1$  or  $-1$  of every spin.

If there are  $N$  spins, then in I it is shown that

$$\kappa = Z^{1/N} = \eta/\xi \quad (3)$$

where  $\eta$  and  $\xi$  are given by the appropriate solution of the matrix equations (1).

In general this solution will be one in which the matrices are infinite-dimensional. However, quite good approximations to  $\kappa$  can be obtained by truncating these matrices and keeping only a few rows and columns. Such approximations correctly give the first few terms in a low- (or high-) temperature expansion. The more rows and columns are kept, the more terms are given correctly. This is the essential idea of this paper.

Here we consider the usual nearest-neighbor Ising model in a magnetic field, with

$$\begin{aligned} w(a, b, a', b') = \exp\{\frac{1}{2}K(ab + bb' + b'a' + a'a - 4) \\ + \frac{1}{4}L(a + b + b' + a' - 4)\} \end{aligned} \quad (4)$$

where  $K$  and  $L$  are positive, being given by

$$K = J/kT, \quad L = H/kT \quad (5)$$

Here the ground-state energy has been subtracted from the Hamiltonian to ensure that

$$w(+, +, +, +) = 1 \quad (6)$$

This is convenient for our purposes, since we shall be obtaining low-temperature expansions, which is equivalent to perturbing about the state in which all spins are positive.

Substituting the expression (4) for  $w$  into (1), the resulting equations can be somewhat simplified by defining

$$\begin{aligned} \bar{F}(a, b) &= e^{K(ab-1)/2 + L(a+b-2)/8} A^{1/2}(a)F(a, b)A^{1/2}(b) \\ \bar{A}(a) &= e^{(K+L/4)(1-a)} A(a) \end{aligned} \quad (7)$$

and

$$\begin{aligned} \bar{\tau}(+, +) &= \bar{\tau}(+, -) = \bar{\tau}(-, +) = 1, & \bar{\tau}(-, -) &= u \\ \bar{\rho}(+) &= 1, & \bar{\rho}(-) &= \mu u^2 \end{aligned} \quad (8)$$

where

$$u = e^{-4K}, \quad \mu = e^{-2L} \quad (9)$$

The equations then become

$$\begin{aligned} \sum_b \bar{\tau}(a, b) \bar{F}(a, b) \bar{A}(b) \bar{F}(b, a) &= \xi \bar{\rho}(a) \{\bar{A}(a)\}^3 \\ \sum_{b, b'} \bar{F}(a, b) \bar{F}(b, b') \bar{F}(b', a') &= \eta \bar{\tau}(a, a') \bar{A}(a) \bar{F}(a, a') \bar{A}(a') \end{aligned} \quad (10)$$

for  $a, a' = +1$  or  $-1$ .

It is convenient to introduce the enlarged matrices

$$C = \begin{pmatrix} \bar{A}(+) & 0 \\ 0 & \bar{A}(-) \end{pmatrix}, \quad H = \begin{pmatrix} \bar{F}(+, +) & \bar{F}(+, -) \\ \bar{F}(-, +) & \bar{F}(-, -) \end{pmatrix}, \quad S = \begin{pmatrix} I & 0 \\ 0 & -I \end{pmatrix} \quad (11)$$

where  $I$  is the identity matrix. Let the elements  $i, j$  of  $C$ ,  $H$ , and  $S$  be  $c_{ij}$ ,  $h_{ij}$ , and  $s_{ij} = s_i \delta_{ij}$ , respectively. Then  $s_i$  has value  $+1$  or  $-1$  depending on the block in which the row and column  $i$  lie. Define

$$\begin{aligned} \tau_{ij} &= 1 & \text{if } s_i \text{ or } s_j &= +1 \\ &= u & \text{if } s_i = s_j &= -1 \end{aligned}$$

and

$$\begin{aligned} \rho_i &= 1 & \text{if } s_i &= +1 \\ &= \mu u^2 & \text{if } s_i &= -1 \end{aligned} \quad (12)$$

Then Eqs. (10) can be written

$$\sum_k \tau_{ik}(HC)_{ik}h_{kj} = \xi\rho_i(C^3)_{ij} \quad \text{if } s_i = s_j$$

$$(H^3)_{ij} = \eta\tau_{ij}(CHC)_{ij}, \quad \text{all } i \text{ and } j$$
(13)

From (1c), both  $C$  and  $H$  are symmetric matrices.

In I it was shown that a basis can normally be chosen in which  $A(+)$  and  $A(-)$  are diagonal matrices. In most of this paper we shall use this representation, so  $C$  is also diagonal, with elements  $c_{ij} = c_i\delta_{ij}$ . Introducing the matrix  $V = H^2$ , we can write Eqs. (13) explicitly as

$$\sum_k \tau_{ik}h_{ik}c_kh_{kj} = \xi\rho_i c_i^3 \delta_{ij} \quad \text{if } s_i = s_j$$
(14a)

$$\sum_k v_{ik}h_{kj} = \eta\tau_{ij}c_i h_{ij}c_j$$
(14b)

$$\sum_k h_{ik}h_{kj} = v_{ij}$$
(14c)

If the matrices  $C$ ,  $H$ , and  $V$  are  $n$  by  $n$ , then  $i$  and  $j$  take the values  $1, \dots, n$ , and the  $k$ -summations are from  $k = 1$  to  $k = n$ .

The normalization of  $C$  and  $H$  is still undetermined. A convenient way to fix it is to require that

$$c_1 = h_{11} = 1$$
(15)

### 3. ITERATIVE DIAGONALIZATION PROCEDURE

In I an iterative method for solving the equations was proposed. In terms of our present notation it can be expressed as follows.

Define  $R$ ,  $U^+$ , and  $U^-$  to be the matrices with elements

$$r_{ij} = (\tau_{ij}c_i/\xi\rho_j c_j^3)^{1/2}h_{ij}$$
(16a)

$$u_{ij}^+ = v_{ij}/(c_i c_j)^{1/2}$$
(16b)

$$u_{ij}^- = v_{ij}/[v_i v_j (c_i c_j)^{1/2}],$$
(16c)

where

$$v_i = 1 \quad \text{if } s_i = +1$$

$$= u^{1/2} \quad \text{if } s_i = -1$$
(17)

Then Eqs. (14a) and (14b) can be written (using the symmetry of  $H$ )

$$\sum_k r_{ki}r_{kj} = \delta_{ij} \quad \text{if } s_i = s_j$$
(18a)

$$\sum_k u_{ik}^+ r_{kj} = r_{ij}(\eta c_j) \quad \text{if } s_j = +1$$
(18b)

$$\sum_k u_{ik}^- r_{kj} = r_{ij}(\eta c_j) \quad \text{if } s_j = -1$$

From (18b) it is apparent that each  $\eta c_j$  is an eigenvalue of  $U^+$  (if  $s_j = +1$ ) or of  $U^-$  (if  $s_j = -1$ ). The column vector  $j$  of the matrix  $R$  is the

corresponding eigenvector. Equation (18a) merely states that eigenvectors of the same matrix should be chosen to be orthonormal.

Given an initial guess at  $\xi$ ,  $\eta$ ,  $C$ ,  $H$ , and  $V$ , the iteration procedure is as follows:

- (i) Calculate  $U^+$  and  $U^-$  from (16b).
- (ii) Diagonalize  $U^+$  and  $U^-$  to obtain the  $r_{ij}$  and  $\eta c_j$  in (18). Use (15) to obtain  $\eta$ , and hence  $c_2, c_3, \dots$
- (iii) Calculate  $\xi^{-1/2} h_{ij}$  from (16a). Use (15) to obtain  $\xi$ , and hence the  $h_{ij}$ . If  $h_{ij}$  is "more accurate" than  $h_{ji}$ , then set  $h_{ji} = h_{ij}$ .
- (iv) Calculate  $v_{ij}$  from (14c). Then repeat.

Note that if  $C$ ,  $H$ , and  $V$  are initially  $n$  by  $n$ , then so are both  $U^+$  and  $U^-$ , so (18) gives  $2n$  eigenvalues  $c_j$ , and  $2n$  column vectors for  $R$ . To obtain the correct infinite-dimensional solution, all of these should in principle be kept, so the new  $C$  and  $R$  are  $2n$  by  $2n$  matrices. The rows of  $R$  corresponding to the  $n$  new eigenvalues should at this stage be set to zero.

Thus the matrices should double in size at each iteration. However, in practice it is useful to repeat each iteration once before expanding the matrices, so as to obtain the correct leading order behavior of the lower elements of  $R$ , and the lower-right elements of  $H$ ,  $V$ ,  $U^+$ , and  $U^-$ .

To see how this works, suppose that  $u$  is small, as it is for low temperatures.

If  $u$  is in fact zero, then all spins must be up, and from Section 5 of I it is obvious that only  $F(+, +)$  and  $A(+)$  are nonzero, and that they are one by one matrices, acting only on the state with all spins up. Thus  $C$ ,  $H$ , and  $V$  are one by one, with  $s_1 = +1$ , and (14) has the trivial solution

$$\xi = \eta = c_1 = h_{11} = v_{11} = 1 \quad (19)$$

Now use this as input to the above iteration procedure, with  $u$  small but nonzero. Keeping only the leading small- $u$  behavior of each matrix element, and setting

$$t = \mu^{1/2} \quad (20)$$

we obtain

- (i)  $U^+ = U^- = (1)$
- (ii)  $C = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix}, \quad S = \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix}, \quad R = \begin{pmatrix} 1 & 1 \\ 0 & 0 \end{pmatrix}$
- (iii)  $H = \begin{pmatrix} 1 & tu \\ tu & 0 \end{pmatrix}$
- (iv)  $V = \begin{pmatrix} 1 & tu \\ tu & t^2 u^2 \end{pmatrix}$

$$\begin{aligned}
 \text{(i)} \quad U^+ &= \begin{pmatrix} 1 & tu \\ tu & t^2u^2 \end{pmatrix}, \quad U^- = \begin{pmatrix} 1 & tu^{1/2} \\ tu^{1/2} & t^2u \end{pmatrix} \\
 \text{(ii)} \quad C &= \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix}, \quad S = \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix}, \quad R = \begin{pmatrix} 1 & 1 \\ tu & tu^{1/2} \end{pmatrix} \\
 \text{(iii)} \quad H &= \begin{pmatrix} 1 & tu \\ tu & t^2u \end{pmatrix} \\
 \text{(iv)} \quad V &= \begin{pmatrix} 1 & tu \\ tu & (t^2 + t^4)u^2 \end{pmatrix} \\
 \text{(i)} \quad U^+ &= \begin{pmatrix} 1 & tu \\ tu & (t^2 + t^4)u^2 \end{pmatrix}, \quad U^- = \begin{pmatrix} 1 & tu^{1/2} \\ tu^{1/2} & (t^2 + t^4)u \end{pmatrix} \\
 \text{(ii)} \quad C &= \begin{pmatrix} 1 & & & \\ & 1 & & \\ & & t^4u^2 & \\ & & & t^4u \end{pmatrix}, \quad S = \begin{pmatrix} 1 & & & \\ & -1 & & \\ & & 1 & \\ & & & -1 \end{pmatrix} \\
 R &= \begin{pmatrix} 1 & 1 & -tu & -tu^{1/2} \\ tu & tu^{1/2} & 1 & 1 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{pmatrix} \\
 \text{(iii)} \quad H &= \begin{pmatrix} 1 & tu & -t^7u^4 & -t^8u^3 \\ tu & t^2u & t^6u^3 & t^7u^2 \\ -t^7u^4 & t^6u^3 & 0 & 0 \\ -t^8u^3 & t^7u^2 & 0 & 0 \end{pmatrix} \\
 &\quad \vdots \\
 R &= \begin{pmatrix} 1 & 1 & -tu & -tu^{1/2} \\ tu & tu^{1/2} & 1 & 1 \\ -t^9u^5 & t^7u^3 & t^2u & t^2u^{1/2} \\ -t^{10}u^{3/2} & t^8u^2 & t^3u^{1/2} & t^3u^{1/2} \end{pmatrix} \\
 \text{(iii)} \quad H &= \begin{pmatrix} 1 & tu & -t^7u^4 & -t^8u^3 \\ tu & t^2u & t^6u^3 & t^7u^2 \\ -t^7u^4 & t^6u^3 & t^6u^3 & t^7u^3 \\ -t^8u^3 & t^7u^2 & t^7u^3 & t^8u^2 \end{pmatrix} \tag{21}
 \end{aligned}$$

The next steps would be to calculate the four by four matrices  $V$ ,  $U^+$ , and  $U^-$ , then the eight by eight matrices  $C$ ,  $R$ , and so on. Note that doubling the size of the matrices does not affect the leading terms of the elements already obtained: for instance, the two by two matrix  $H$  given above is the top-left block of the four by four matrix  $H$ .

One very useful fact emerges from this procedure: the rows and columns can always be ordered so that

$$s_i = (-1)^{i-1} \tag{22}$$

and, to leading order in  $u$ ,

$$R = \begin{pmatrix} 1 & 1 & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & 1 & 1 & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & 1 & 1 & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & 1 & 1 & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \end{pmatrix} \tag{23}$$

the dots denoting elements that vanish when  $u = 0$ . These two requirements actually fix the ordering of the rows and columns. We shall call this the "natural" ordering.

For a given integer  $i$ , let  $i'$  be defined by

$$i' = \text{Int}[\frac{1}{2}(i + 1)] \tag{24}$$

Then, from (23),

$$\begin{aligned} r_{i',i} &= 1 + \mathcal{O}(u) \\ r_{ji} &= o(u) \quad \text{if } j \neq i' \end{aligned} \tag{25}$$

**4. LEADING ORDER EQUATIONS FOR THE  $c_i$**

From (25), for  $j = i$  the summation in (18a), and therefore also in (14a), is dominated for small  $u$  by the term  $k = i'$ . Using the symmetry of  $H$ , and the fact that  $\xi = 1 + \mathcal{O}(u)$ , to leading order (14a) therefore gives

$$\tau_{ii'}c_i h_{ii'}^2 = \rho_i c_i^3 \tag{26a}$$

Further, if  $j = i$  in (14b), or if  $j = i'$  in (14b) or (14c), the summation on the rhs is again dominated by the term  $k = i'$ . Since  $\eta = 1 + \mathcal{O}(u)$ , it follows that to leading order

$$\begin{aligned} v_{ii'} h_{ii'} &= \tau_{ii'} c_i h_{ii'} c_i \\ v_{ii'} h_{i'i'} &= \tau_{ii'} c_i h_{ii'} c_{i'} \\ h_{ii'} h_{i'i'} &= v_{ii'} \end{aligned} \tag{26b}$$

These equations can be solved sequentially, giving the leading order behavior of  $c_1, c_2, c_3, \dots$ . The natural way to write the result is to go back to the original matrices  $A(+)$  and  $A(-)$ , whose diagonal elements are  $\rho_i^{1/4} c_i$ , and to use a binary, or spin, representation of the indices, setting

$$\begin{aligned} i &= \{\sigma_1, \sigma_2, \sigma_3, \dots\} \\ &= 1 + \frac{1}{2}[(1 - \sigma_1) + 2(1 - \sigma_2) + 4(1 - \sigma_3) + 8(1 - \sigma_4) + \dots] \end{aligned} \tag{27}$$



where  $\sigma_1, \sigma_2, \sigma_3, \dots$  take the values  $+1$  or  $-1$ . Thus the value 1 of the index  $i$  corresponds to  $\sigma_1 = \sigma_2 = \sigma_3 = \dots = +1$ , i.e., all spins up. The value 2 corresponds to  $\sigma_1$  being down, the rest up; and so on.

From (24) it follows that if  $i$  is given by (27), then

$$i' = \{\sigma_2, \sigma_3, \sigma_4, \dots\} \tag{28}$$

and the solution of (26) is found to be

$$\rho_i^{1/4} c_i = \exp\left\{ \frac{1}{4} L(\sigma_1 - 1) + \sum_{r=1}^{\infty} [(2r - 1)K(\sigma_r \sigma_{r+1} - 1) + 2rL(\sigma_{r+1} - 1)] \right\} \tag{29}$$

Note that when  $L = 0$  (no magnetic field) this expression can be written as a direct product in terms of the spins  $\mu_r = \sigma_r \sigma_{r+1}$ , giving

$$\mathcal{A} = \rho^{1/4} C = \begin{pmatrix} 1 & 0 \\ 0 & u^{1/2} \end{pmatrix} \otimes \begin{pmatrix} 1 & 0 \\ 0 & u^{1/4} \end{pmatrix} \otimes \begin{pmatrix} 1 & 0 \\ 0 & u^{1/4} \end{pmatrix} \otimes \dots \tag{30}$$

It has been shown<sup>(8)</sup> that this result is exact for all temperatures  $T$  less than  $T_c$ , provided  $u$  is replaced by the nome of the elliptic functions that occur in the exact solution of the zero-field Ising model.<sup>(9)</sup>

### 5. SIMPLIFIED ITERATIVE PROCEDURE

The iterative method of solution given in Section 3 is quite general, but rather cumbersome. Fortunately we found that for the nearest-neighbor Ising model it can be enormously simplified. First write Eq. (14a), with  $j = i$ , as

$$\tau_{ii} \cdot c_i h_{ii}^2 = \xi \rho_i c_i^3 - \sum_{k \neq i'} \tau_{ik} h_{ik} c_k h_{ki} \tag{31a}$$

and write (14b) and (14c) as

$$\begin{aligned} v_{ij} h_{jj} - \eta \tau_{ij} c_i h_{ij} c_j &= - \sum_{k \neq j} v_{ik} h_{kj} \\ v_{ij} - h_{ij} h_{jj} &= \sum_{k \neq j} h_{ik} h_{kj} \end{aligned} \tag{31b}$$

First calculate the  $c_i, h_{ii}$  (up to some maximum value of  $i$ ) from (15) and the leading order equations (26). Set  $h_{i'i} = h_{ii}$  and set all other matrix elements to zero. Now proceed as follows:

- (i) Calculate  $v_{11}$  from (14c).
- (ii) Calculate  $\eta$  from (14b), with  $i = j = 1$ .
- (iii) Calculate  $\xi$  from (14a), with  $i = j = 1$ .
- (iv) Calculate  $\kappa = \eta/\xi$ .

Set  $i = 2$ .

(v) Calculate  $v_{i'}$  from (14c). Set  $v_{i'i} = v_{i'}$ .

(vi) Calculate  $c_i$  from (14b), with  $i = i'$ .

(vii) Calculate  $h_{i'}$  from (31a). Set  $h_{i'i} = h_{i'}$ .

(viii) Regard (31b) as two linear equations for the  $v_{ij}$  and  $h_{ij}$  explicitly occurring on the lhs, with "known" coefficients involving  $c_i$ ,  $c_j$ , and  $h_{jj}$ . For  $j = 1, \dots, i$ , but not equal to  $i'$ , solve these equations for  $v_{ij}$  and  $h_{ij}$ . Set  $v_{ji} = v_{ij}$  and  $h_{ji} = h_{ij}$ .

Now increase  $i$  by one, and repeat steps (v)–(viii) up to the desired maximum value of  $i$ . Then go back to (i) and repeat the whole procedure.

Basically, this is the procedure we have used to obtain the perturbation expansion solution of the equations in powers of  $u$ , except that we did not necessarily use precisely the sequence indicated.

## 6. EXPANSION IN POWERS OF $u$

As is well known,<sup>(10)</sup>  $\kappa$  can be expanded in a power series in  $u$ :

$$\begin{aligned} \kappa &= 1 + \mu u^2 + 2\mu^2 u^3 + (\mu^4 + 6\mu^3 - 2\mu^2)u^4 + \dots \\ &= \sum_{r=0}^{\infty} a_r u^r \end{aligned} \quad (32)$$

where each coefficient  $a_r$  is a polynomial in  $\mu$  with integer coefficients. The other variables  $\xi$ ,  $\eta$ ,  $h_{11}$ ,  $h_{12}, \dots, v_{11}$ ,  $v_{12}, \dots$  in our equations can similarly be expanded; for instance, any element  $h_{ij}$  of  $H$  can be expanded in the form

$$h_{ij} = u^{l_{ij}} \{ h_{ij0} + h_{ij1}u + h_{ij2}u^2 + \dots \} \quad (33)$$

where  $l_{ij}$  is a nonnegative integer and the coefficients  $h_{ijr}$  are functions only of  $\mu$ . The procedure of Section 5 can be used to systematically obtain all such coefficients, in particular the coefficients  $a_r$  in (32).

The usefulness of the present approach lies in the fact that to obtain the first  $m$  coefficients in (32) it is only necessary to expand a finite number of elements of  $H$  and  $V$  (all the rest can be taken to be zero), and no more than  $m$  coefficients are needed in any element. To see this, consider, for example, Eq. (14a) with  $i = j = 1$ . This equation can be regarded as defining  $\xi$ . Using (15), we can write it as

$$\xi = 1 + c_2 h_{21}^2 + c_3 h_{31}^2 + c_4 h_{41}^2 + \dots \quad (34)$$

Using the small- $u$  behavior given in Section 3, we obtain the orders of magnitude of the various terms in (34) as

$$\xi = 1 + \mathcal{O}(u^2) + \mathcal{O}(u^{10}) + \mathcal{O}(u^7) + \dots \quad (35)$$

**Table 1. Variables Needed in Calculating  $\kappa$  to Order  $7^a$  and the Maximum Number of Terms Needed in the Expansion of Each Variable**

Variable	Maximum number of terms needed	Variable	Maximum number of terms needed	Variable	Maximum number of terms needed
$v_{11}$	8	$c_2$	6	$h_{14}$	2
$\eta$	8	$h_{22}$	5	$c_{14}$	2
$\xi$	8	$v_{22}$	4	$h_{44}$	1
$v_{12}$	6	$v_{24}$	2	$v_{14}$	1
$h_{12}$	6	$h_{24}$	2		

<sup>a</sup> I.e., the first eight terms. Recall that  $c_1$  and  $h_{11}$  are fixed to be one.

The general trend is for the powers of  $u$  to increase: the largest term omitted in (35) is actually of order  $u^{12}$ . Thus, if we wish to obtain  $\xi$  to order  $u^7$  (say) from this equation, we shall need

$c_2$  and  $h_{21}$  to relative order  $u^5$  (first six coefficients)  
 $c_4$  and  $h_{41}$  to leading order only (first coefficient)

All other matrix elements occurring in this equation (including  $c_3$  and  $h_{31}$ ) are negligible to this order.

Of course, to obtain  $\kappa$  to order  $u^7$ , we need both  $\xi$  and  $\eta$  to this order, so it is also necessary to look at the equation used to calculate  $\eta$ , and then at the equations used to determine all the variables that are needed in calculating  $\xi$  and  $\eta$ , and so on. Even so, we find that only 14 variables are needed, and for many of these only the first one or two terms in their expansions are needed, as is shown in Table I.

Note in particular that only elements occurring in rows and columns one, two, and four are needed. All other elements can be taken to be zero. Thus, in using the iterative procedure of Section 5 we could stop at  $i = 4$ , and ignore  $i$  (or  $j$ ) = 3, provided we need  $\kappa$  only to order  $u^7$ .

If we want  $\kappa$  to a higher order, then we of course need more rows and columns of the matrices. For instance, to order  $u^{11}$  we need elements in rows and columns one, two, three, four, and eight. Any element  $c_i$ ,  $h_{ij}$ ,  $v_{ij}$  with either  $i$  or  $j$  not equal to one of these values can be ignored.

More generally, we found empirically the following simple rule: to calculate  $\kappa$  to order  $u^{2m+1}$  we need only those rows and columns  $i$  for which  $\rho_i^{1/2}c_i^2 \geq u^m$ . From (29), this implies that the  $\sigma_1, \sigma_2, \dots$  in (27) must satisfy

$$\alpha_i \equiv \sum_{r=1}^{\infty} (2r-1)(1-\sigma_r\sigma_{r+1}) \geq 2m \quad (36)$$

Table 2. The First 19 Values of  $\alpha_i$  in Nondecreasing Order<sup>a</sup>

<i>i</i>	$\alpha_i$	<i>i</i>	$\alpha_i$	<i>i</i>	$\alpha_i$	<i>i</i>	$\alpha_i$
1	0	7	12	32	18	9	24
2	2	16	14	13	20	29	24
4	6	5	16	31	20	63	24
3	8	15	16	14	22	10	26
8	10	6	18	64	22		

<sup>a</sup> This  $\alpha_i$  is the leading power of  $u$  in the expansion of  $\rho_i c_i^4$ .

This rule makes good sense. The variational expression (31a) for  $\kappa$  in I contains a factor

$$r_1 = \sum_a \text{Tr } A^4(a) \tag{37}$$

which in our present notation becomes

$$r_1 = \sum_i \rho_i c_i^4 \tag{38}$$

Thus the rule (36) is equivalent to stating that if the contribution of  $c_i$  to  $r_1$  is negligible (to the required order  $u^{2m+1}$ ), then row  $i$  and column  $i$  may be deleted from the matrices.

In Table II the first 19 values of  $\alpha_i$ , arranged in nondecreasing order, are given. It can be seen that to obtain  $\kappa$  to order  $u^{23}$  we needed 15 rows and columns of the matrices. To obtain  $\kappa$  to order  $u^{25}$  we would need 18 rows and columns.

### 7. TECHNICAL MODIFICATIONS

The coefficients in the expansion of  $\kappa$  are themselves polynomials in  $\mu$ , with integer coefficients. It would obviously be a considerable computational simplification if this were true of all coefficients of powers of  $u$  that occur, for instance, the  $h_{ijr}$  in (33).

We ensured this by overcoming two obstacles. The first is that step (vii) of Section 5 involves taking a square root, which can produce half-integer leading powers of  $u$  and  $\mu$  (as is evident in Section 3), and noninteger coefficients. To avoid this we replaced  $H$  and  $V$  in (14) by  $P^{1/2}HP^{1/2}$  and  $P^{1/2}VP^{1/2}$ , where  $P$  is a diagonal matrix. The elements  $h_{ii'}$  can then be chosen arbitrarily, and (31a) regarded instead as a linear equation for  $p_i$ .

The other difficulty is in step (viii), which involves dividing by the determinant of the coefficients of  $v_{ij}$  and  $h_{ij}$  in (31b), namely

$$\Delta_{ij} = \eta\tau_{ij}c_i c_j - h_{jj}^2 \tag{39}$$

Let  $k = 2j$  if  $i$  is even,  $2j + 1$  if  $i$  is odd. Then  $j = k'$ , and from (26b) it follows that to leading order

$$\Delta_{ij} = \tau_{ij}c_i c_j - \tau_{kj}c_k c_j = \tau_{ij}c_j(c_i - c_k) \quad (40)$$

since  $s_i = s_k$ .

Provided that  $c_i$  is not of the same order as  $c_k$ ,  $\Delta_{ij}$  is to leading order of the form  $\pm \mu^{2p}u^n$ , and there is no problem in dividing by it.

Since  $s_i = s_k$ , it is also true that  $\rho_i = \rho_k$ . Thus  $c_i$  is of the same order as  $c_k$  iff  $\alpha_i = \alpha_k$ , where  $\alpha_i$  is given by (36). Since  $j = i'$  is excluded in step (viii),  $i$  and  $k$  are distinct.

From Table II it is apparent that the lowest seven  $\alpha_i$  are unequal. To order 15 in  $\kappa$ , only the rows and columns corresponding to these  $\alpha_i$  are needed in the calculation, so  $c_i$  and  $c_k$  in (40) are always of different orders, and all is well. In fact, (31b) becomes effectively two independent equations: one for  $h_{ij}$ , the other for  $v_{ij}$ .

However, when calculating  $\kappa$  to higher order, values of  $i$  and  $k$  for which  $\alpha_i = \alpha_k$  ( $i \neq k$ ) are needed; the first are 5 and 15. In these cases we allowed the off-diagonal element  $c_{ik}$  ( $=c_{ki}$ ) of  $C$  to be nonzero, and set  $h_{ij}$  (for  $i < k$ ) to zero. For  $i < k$ , step (viii) was then replaced by a calculation of  $v_{ij}$  and  $c_{ik}$ . For  $i > k$ ,  $h_{ij}$  was calculated from (14a),  $v_{ij}$  from (14c).

Since  $C$  is no longer diagonal, the equations were of course appropriately modified, starting from the basis-independent equations (13). Fortunately it remained true that  $C$  was "near-diagonal," in the sense that to leading order in  $u$  its diagonal elements were its eigenvalues. Thus the discussion of Section 4, for instance, remains true, provided  $c_i$  is understood to be the diagonal element  $c_{ii}$  of  $C$ .

## 8. COMPUTATIONAL PROCEDURE

The procedure for obtaining series coefficients breaks up into seven main stages

(i) Determine the "structure" of the equations and the leading powers of the  $c_i$ , as described in Section 4.

(ii) Obtain a specification for which equations determined which matrix elements. This is given in Section 5. For each new matrix element introduced in Section 7, one of the original matrix elements is fixed and this is done in such a way as to preserve the essential structure of the iterative procedure described in Section 5.

These first two stages were carried out by hand.

(iii) Work through the equations as in Section 5 to determine the leading powers of  $u$  in the expansion of each matrix element.

(iv) Determine the relative order needed in each matrix element to obtain  $\kappa$  to the desired order  $m$ .

(v) Determine the sequence in which the individual steps (one for each variable) in Section 5 should be performed. This sequence was required to produce one new term in one matrix element at each step.

These three stages were carried out using a DEC-10 computer. The calculations required only short runs of comparatively small Fortran programs. Steps (iii) and (iv) were carried out using up to 50 rows and columns of the matrices so as to be reasonably sure that no significant elements had been ignored.

(vi) Calculate successive coefficients of the matrix elements in the order obtained from (v).

(vii) As a check, substitute the solutions obtained into every matrix equation [including those which were not needed in steps (iii)–(vi)] to check that each equation is satisfied to the appropriate order in  $u$ .

By dividing the calculations into stages in this way we ensured that only the short calculations of stages (iii)–(v) involved iterative procedures. In the longer calculations of stage (vi) each coefficient in each matrix element was calculated directly rather than being obtained as the limit of a sequence of improvements.

## 9. COMPUTATIONAL DETAILS

The most critical part of any computer calculation involving algebraic manipulation is normally the design of the data structures. Dividing the problem into stages as described in Section 8 enabled us to achieve some considerable simplifications.

For stages (iii)–(v) only a limited amount of information was needed for each matrix element (leading power, required order, known order) and so the various properties could be conveniently stored using Fortran arrays. Each of the stages (iii)–(v) involved iterative procedures. Each equation from Section 5 was examined in turn and, if possible, used to refine the current quantity being calculated. This whole process was repeated until no further refinements occurred.

Stage (iii) calculated leading powers [e.g.,  $l_{ij}$  in (33)]. The starting point for the iteration was to assume that the leading powers were arbitrarily large in all variables except the “fixed” variables and the  $c_i$ .

Stage (iv) calculated the required orders. The initial stage was a specified required order for  $\kappa$ . Other variables were initially specified as being not required at all.

Stage (v) operated by assuming that all earlier calculations had been

performed to specified orders. The program then searched cyclically through the equations, applying the following procedure:

(a) Is the variable needed to one more order? If not, go on to the next equation.

(b) Can the variable be calculated to one more order at this stage? (I.e., are all the other variables in the equation known to sufficiently higher order?) If so, record this as the next step in the sequence of calculations and regard the variable as having been calculated.

Since the procedure of Section 5 is purely empirical, it could have happened at some stage that there were variables to update but no single equation which determined any one of them (i.e., we would have had to solve simultaneous equations in order to proceed). Fortunately this did not occur.

The knowledge of this iteration sequence for obtaining coefficients was exploited in the design of stage (vi).

The calculation of  $\kappa$  to order 23 involved about 270 matrix elements (and the variables  $\kappa$ ,  $\xi$ , and  $\eta$ ). Each of these quantities was a power series in  $u$  with from one to 24 terms. The coefficients were expressions of the form  $\mu^a \sum_{m=0}^n c_m \mu^m$  with  $n$  ranging from zero to over 100 (the leading power  $a$  was allowed to be negative). The number of  $c_m$  in all the terms of all the matrix elements grew roughly exponentially with the order to which  $\kappa$  was calculated, 70,000 numbers being required at order 23. Because of the sequential nature of the calculation it was possible to store these numbers in a linear array so that  $\mu^a \sum_{m=0}^n c_m \mu^m$  was represented by the sequence  $(n, a, c_0, \dots, c^n)$  and this sequence was stored immediately after the previous such sequence. Since each such polynomial was calculated correctly without any subsequent revisions and required for all subsequent orders, there was no need of any complicated memory management to allow for reuse of space formerly occupied by temporary intermediate quantities. The polynomials for various powers of  $u$  were located by an array of pointers associated with each matrix element.

Like the memory requirements, the execution time and the maximum integers occurring grew exponentially with the order of the calculation. It took about 16 sec of CPU time to reproduce the results of Sykes *et al.*<sup>(7)</sup> and slightly more than an hour to obtain  $\kappa$  to order 23. At order 18 certain coefficients exceed  $2^{35} - 1$ , the maximum integer allowed by our Fortran system. The calculations were therefore performed using modular arithmetic. The whole program was run twice, once with calculations being performed modulo  $2^{35}$  and once with calculations being performed modulo 3937, so that the results in the appendix are correct modulo  $2^{35} \times 3937$ . If the observed exponential growth in the size of the maximum coefficient is preserved through to order 23, then the values tabulated will be correct without any additional

multiples of  $2^{35} \times 3937$ . An additional reason for believing that such multiples are absent is that for  $\mu = \pm 1$ , both  $\kappa$  and  $\partial\kappa/\partial\mu$  agree with the known exact solutions.<sup>(9,11,12)</sup>

## 10. VARIATIONAL APPROXIMATIONS

We emphasize again that we have used the exact infinite-dimensional matrix equations (1), calculating all matrix element coefficients necessary to obtain  $\kappa$  to order  $u^{23}$ .

At the same time, it is interesting to use our methods to test the variational approximations proposed in I. These are obtained by restricting the matrices in (1) to be of finite size. The natural sequence of such approximations is to take the matrices to be 1 by 1, 2 by 2, 4 by 4, 8 by 8, etc.; and to be given at low temperatures as in Section 3. Tsang<sup>(6)</sup> has investigated these approximations numerically for the zero-field Ising model, and has found that they converge rapidly (extremely rapidly away from the critical point) to the known exact values.

We can now answer the question: how many terms in the expansion of  $\kappa$  does a given approximation correctly reproduce?

It was easy to modify our program so as to keep only elements occurring in a given approximation, and to then compare the resulting series for  $\kappa$  with the exact one.

The 1 by 1 approximation is that of Kramers and Wannier.<sup>(4)</sup> This correctly gives  $\kappa$  to order  $u^5$ , and gives the coefficient of  $u^6$  correctly except that it omits the term  $\mu^9 u^6$ . Thus

$$\kappa_{\text{exact}} - \kappa_{1 \times 1} = \mu^9 u^6 + \mathcal{O}(u^7) \quad (41a)$$

Similarly, we have found that

$$\begin{aligned} \kappa_{\text{exact}} - \kappa_{2 \times 2} &= \mu^{25} u^{10} + \mathcal{O}(u^{11}) \\ \kappa_{\text{exact}} - \kappa_{4 \times 4} &= \mu^{49} u^{14} + \mathcal{O}(u^{15}) \\ \kappa_{\text{exact}} - \kappa_{8 \times 8} &= \mu^{81} u^{18} + \mathcal{O}(u^{19}) \end{aligned} \quad (41b)$$

From these results it is apparent that the leading error in the  $2^{n-1}$  by  $2^{n-1}$  approximation is  $\mu^{(2n+1)^2} u^{4n+2}$ . Graphically, this is the contribution to  $\kappa$  of a  $2n+1$  by  $2n+1$  square, consisting entirely of reversed spins.

## APPENDIX

The series expansion for  $\kappa$  is of the form

$$\kappa = 1 + \sum_{n=2}^{\infty} \sum_m C(n, m) u^n \mu^m$$





		C(11,6)		TO		C(11,30)			
5204	-65104	151574	-694	-65862	-87948	-49786	-17472		
13272	25458	31394	28974	24000	17746	12176	7574		
4472	2408	1208	560	238	88	30	8		
	2								

		C(12,6)		TO		C(12,36)			
-1362	70850	-467359	649535	262160	-87840	-378393	-337810		
-242384	-83084	12470	88700	119884	128778	117766	99290		
75882	55076	37234	23814	14364	8238	4410	2244		
1054	470	187	68	22	6	1			

		C(13,7)		TO		C(13,42)			
-39030	732764	-2932576	2228858	2029462	874668	-1014862			
-1545118	-1625216	-1051706	-589506	-100010	213582	429998			
522638	549068	504642	435766	350336	267222	193180			
133968	88290	55970	33738	19574	10784	5664			
2816	1332	584	238	88	30	8			
	2								

		C(14,7)		TO		C(14,49)			
8670	-639433	6311938	-16244768	4560830	10051601				
9549646	762288	-4249586	-7695965	-6881592	-5583312				
-3337080	-1518502	97156	1164396	1945588	2281417				
2382596	2255598	2006540	1682052	1352688	1037676				
768638	546306	375856	249154	159656	98522				
58838	33768	18664	9866	5014	2408				
1106	470	187	68	22	6				
	1								

		C(15,8)		TO		C(15,56)			
296652	-7804442	47256224	-78778800	-10768506	32372408				
59058342	31112876	4952616	-23743438	-31567608	-33797354				
-27241336	-19920878	-11449760	-4791266	1316882	5415648				
8391488	9972394	10580136	10279976	9481042	8287220				
6980988	5647102	4426656	3356992	2473336	1766316				
1227956	828890	544458	346994	215208	129258				
75440	42520	23178	12160	6136	2960				
1360	584	238	88	30	8				
	2								

		C(16,8)		TO		C(16,64)			
-57253	5685542	-78352726	313892342	-322579472					
-186465885	12493642	261194858	238197716	159972553					
-597278	-86868766	-148295915	-153278297	-140530480					
-108483798	-78593018	-44988760	-18303116	5156834					
22564319	35587123	43185150	47169002	47364155					
45256582	41190974	36188632	30705631	25323304					
20273390	15829110	12041549	8948590	6487288					
4599332	3182598	2154074	1423134	918726					
578554	355542	212810	124132	70233					
38620	20524	10558	5202	2468					
1106	470	187	68	22					
	6								

		C(17,9)		TO		C(17,72)			
-2278538	80010676	-679161356	1863094888	-993191542					
-1251265124	-764445582	724510014	1183548008	1274083894					
635252528	127063826	-379872674	-616220230	-729611390					
-681225430	-601802848	-462209986	-333441648	-202229512					
-90986820	8428644	84160308	144560572	183938370					
208594416	217550716	215438532	203846368	186544548					
165178696	142441448	119644950	98244398	78820104					
61956052	47670848	35977028	26611628	19314722					
13746848	9600928	6574570	4418162	2909010					
1877982	1186826	734714	444422	262906					
151632	85244	46600	24738	12696					
6300	2992	1360	584	288					
88	30	8	2						

C(18,9) TO C(18,81)			
388802	-50032548	916955220	-5217511816
9834974207	-1089145506	-5657415098	-7098109106
-487090066	3635914388	6838712692	5540059481
3680485502	831342834	-1147699828	-2666288478
-3197910140	-3404412644	-3082431138	-2656113322
-2087698748	-1546743800	-993051812	-521524459
-87170874	259626592	547690090	756159946
902055898	981708972	1011770298	995157736
946239371	871933652	783431182	686674998
589385362	495302608	408530636	330685268
263068892	205658638	158148838	119586158
89003823	65162530	46959374	33290564
23229701	15940820	10762790	7143314
4660592	2986678	1879750	1160328
702578	416448	241610	136848
75685	40712	21304	10770
5270	2468	1106	470
187	68	22	6
1			

C(19,10) TO C(19,90)			
17649910	-797699944	9016362186	-36018566176
45188788806	13621335208	-14707405668	-42179699380
-22532767840	-1569288086	25232887974	30719299520
29745477974	18615039164	7925920732	-3076407410
-9591429048	-14406378468	-15739114470	-15741068066
-14212502540	-12318554234	-9873794544	-7587998260
-5225244528	-3152960096	-1216458816	414413968
1814578926	2900487922	3739479444	4297607820
4629244778	4741404944	4686737324	4486638124
4188731988	3817870916	3409991942	2986345974
2569772506	2173560256	1809591182	1482920164
1197509370	952833304	747583408	578263006
441254780	332060818	246552076	180569152
130470700	92978850	65362432	45302620
30963148	20855388	13843842	9049282
5824898	3688490	2297646	1405942
845040	498056	287682	162568
89800	48344	25338	12880
6336	2992	1360	584
238	88	30	8
2			

C(20,10) TO C(20,100)			
-2699202	436976042	-10273440219	78353373965
-224603332620	170177308196	137645380565	30290040193
-181767876286	-176499399732	-118585422851	33966625668
113112711312	162942828110	144892167071	109025803836
52019575364	7935035690	-33346637431	-57056817287
-72044727940	-75529606284	-74313139558	-67156106274
-58949700218	-48584738492	-38697422840	-28508502848
-19224958776	-10399824286	-2738436906	4111367087
9755582174	14392370794	17858017887	20343275756
21812028152	22462088640	22349550232	21655588075
20482940924	18984024358	17260822518	15431749461
13571789098	11760048162	10042540600	8460370720
7032090196	5771299776	4676825349	3744177562
2961346430	2314740106	1788009488	1365272026
1030329734	768675138	566798557	413139584
297596928	211864634	149017209	103558802
71074110	48172590	32228382	21278938
13857418	8899228	5631354	3510146
2153196	1299326	770133	448272
255710	142900	78009	41580
21540	10846	5270	2468
1106	470	187	68
22	6	1	

	C(21,11)	TO	C(21,110)		
	-137674532		7785746552	-112888535288	612376056680
	-1261409345442		423106621732	801825413332	704180055914
	-472416181748		-889395776028	-1021024867678	-395226054492
	115128451484		611780411810	769125941340	778247147438
	581264541660		378018576704	130274078330	-56645505196
	-210575498342		-298783105656	-354043993498	-363169036964
	-355447107466		-324809631118	-289243215724	-245498356166
	-202439064366		-157512872880	-115950878666	-75563836072
	-39213719214		-5815541354	22949974670	47885535776
	67989446690		83954158250	95419796290	103015575062
	106861414854		107591334036	105552425648	101387623842
	95499032950		88445155468	80608543682	72415666818
	64153016790		56108367452	48459035782	41360450420
	34893724540		29112899304	24024038986	19615962248
	15848336942		12673741034	10031524258	7860845428
	6098011504		4683766622	3561595390	2681586246
	1998818468		1475082080	1077583166	779248172
	557695446		395006668	276808518	191907360
	131574666		89207692	59782024	39593052
	25906410		16731882	10666906	6709210
	4159C25		7541224	1528112	903904
	525376		299750	167600	91728
	49008		25542	12920	6336
	2992		1360	584	238
	88		30	8	2

	C(22,11)	TO	C(22,121)		
	19076006		-3794770713	111304562027	-1092704834228
	4346652233232		-6291768217070	-376126004360	3129928307620
	5592658217298		679016122604	-2724759534469	-5789007505314
	-4382809075566		-2307752907687	794745448158	2699292204678
	3954323197056		3850259185456	3375918830835	2306290801088
	1282990166282		242272413516	-526697708097	-1153904785370
	-1502912104262		-1721524481865	-1758761536061	-1722633811538
	-1597795341798		-1447506956370	-1259323433439	-1072381885192
	-874903651924		-686995664340	-501395669362	-330299440430
	-168407379252		-23992189363	106238437455	217467942226
	311633846638		386664886313	444402432861	484449002118
	509133385060		519203696700	517094841000	504300209966
	483195403146		455421545217	423067326875	387633978474
	350726691968		313517449971	277107077201	242244854088
	209576736204		179469511693	152190239266	127815919430
	106347020794		87667941990	71620746856	57986981032
	46537111248		37020720378	29195990553	22825821468
	17692629696		13595524004	10357675690	7822695960
	5857133378		4347091080	3198142752	2331913666
	1685113960		1206603136	856029487	601590324
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	88896396		58762848	38411074	248180662
	15841458		9985054	6212410	3811952
	2305732		1373310	805061	463756
	262362		145456	78965	41840
	21624		10846	5270	2468
	1106		470	187	68
	22		6	1	

		C(23, 12) TO	C(23, 132)		
1080178538	-74731542218	1351003453762	-9503167548524		
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-191459054670	399873582720	925320442076	1371356526908		
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2500308625556	2529044171728	2507995388538	2443452302656		
2344334766176	221754998498	2071056094176	1910986572650		
1743783003478	1574261974430	1407015953008	1245329036872		
1092038934718	948961018146	817468033792	698172964190		
591348668150	496769408092	413983573728	342261568638		
280767712426	228541284508	184612447588	147993501574		
117745607452	92974018006	72865154256	56676557478		
43754944118	33524837122	25493281372	19238482582		
14407761188	10706769444	7894797574	5775520084		
4191594878	3017463414	2154461718	1525425028		
1070902030	745270346	514072144	351367848		
237929952	159565440	105960218	69643618		
45293968	29134370	18528374	11642842		
7226144	4426312	2674384	1592464		
933808	538576	305258	169712		
92456	49232	25586	12920		
6336	2992	1360	584		
238	88	30	8		
2					

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